HEARING AID

BACKGROUND OF THE INVENTION

5 ### 1. Field of the Invention

The present invention relates to a hearing aid that improves clarity by minimizing the sense that sounds instantly become louder, eliminating the
10 metallic ring to sounds, and so forth.

2. Description of the Related Art

The process by which sound waves are recognized
15 by our auditory system is generally considered to be extremely complex, but to summarize this process, sound waves travel through a conducting system consisting of the external ear canal, the eardrum, the auditory ossicle, the cochlea, hair cells, nerves,
20 and brain cells, where the sound waves are recognized. Within this conducting system, the external ear canal and eardrum are called the outer ear, the eardrum and auditory ossicle are called the middle ear, and the cochlea and hair cells are called the inner ear.
25 A hearing impairment therefore occurs when any of the functions is diminished in this conducting system, and the symptoms will vary, as will the

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method of dealing with them, depending on which function is diminished and to what extent.

The typical form of senile deafness is an overall decrease in function, including brain function, making it difficult to hear weak sounds.

Figure 7 is a graph of equisignal curves of the loudness of sound in humans with normal hearing. The horizontal axis is the frequency (Hz), and the vertical axis is the sound pressure level (dB). Sound pressure level will hereinafter be abbreviated as SPL.

The curves in the graph are known as Fletcher-Manson curves, and the hatched area in the figure indicates the distribution of acoustic energy in a typical conversation. The dashed line labeled "minimum audible level" is a curve corresponding to a human with normal hearing, but in the elderly this is higher on the graph, as with the curve indicated by the dashed line labeled "senile deafness minimum audible level." This senile deafness minimum audible level varies from person to person, so the curve in the graph should be viewed as just an example.

As can be seen from the acoustic energy distribution in a typical conversation, a person with senile deafness is only able to hear about half of the sounds in the voice spectrum which a person with normal hearing is able to hear, so even though the

sounds may be perceptible, the hearer cannot make out
the words.

With the example shown in the graph, if the
acoustic level is raised about 50 dB by a hearing aid,
the voice spectrum of conversation will be more or
less reach the audible level, allowing the wearer to
understand the words, but sounds of, say, 80 dB,
which are encountered on an everyday basis, become
130 dB, which is so loud as to be uncomfortable.

The highest level that a person with normal
hearing is able to stand is about 130 dB, and is said
to be between 120 and 130 dB for a person who is hard
of hearing, which would seem to be about the same,
but in fact the level is often much lower.

Figure 8 is a graph of the formants of Japanese
vowels. The horizontal axis is the first formant
(kHz), and the vertical axis is the second formant
(kHz) (see Rika Nenpyo, p. 491, published by Maruzen,
November 30, 1985).

What Figure 8 tells us is that for the Japanese
vowels "A", "I", "U", "E", and "O" to be clearly
distinguished, for example, the second formant must
be reliably transmitted with respect to the first
formant.

Figure 9 is a table of typical values for
various sounds and their corresponding formant
frequencies. According to this table, the second

formant frequency varies between 1.5 and 7.7 times with respect to the first formant frequency, but if it is not reliably transmitted, the hearer cannot distinguish between A, I, U, E, and O.

In general, the level of the second formant is about 20 to 40 dB lower than the level of the first formant, so even if the first formant can be heard, it is difficult to hear the second formant, and to make matters worse, there is usually a dramatic drop in the perception of high frequencies with a person with senile deafness, as indicated by the dashed line in Figure 7, and this makes it even more difficult to hear the second formant, in which case even though the person may be able to hear the first formant, he does not understand what is being said.

Conventional Approach 1

Because of the above situation, one thing conventional hearing aids had in common was that they raised the level of the second formant high enough to be audible, but while employing this means does indeed work fairly well with mild deafness, with more severe deafness the level of the first formant often exceeds 100 dB, which sounds loud to the wearer.

Conventional Approach 2

Raising the degree of amplification of high

frequencies has been accomplished by using a tone
control circuit, and while this is effective with
persons of mild deafness, with a more severe case of
deafness, if the frequency of the first formant is
high, the first formant level can rise over 100 dB
and become painful, and as a result the wearer hears
a so-called ringing noise.

Conventional Approach 3

Automatic volume adjusting circuits are
frequently used to keep the volume below 100 dB by
immediately lowering the gain if a loud sound over
100 dB should come in. Various methods have been
developed for shielding the wearer from fluctuations
in sound level by optimizing the attack time and
release time, but if someone should suddenly shout
during a conversation, the level is lowered to the
point that it sounds as if the sound source is far
away, and this is particularly undesirable when
listening to sounds through a stereo audio device
because the sensation of a fixed position is lost and
the location of the sound source seems to float
around.

SUMMARY OF THE INVENTION

It is an object of the present invention to

provide a hearing aid which amplifies voices so that they can be clearly understood but do not sound overly loud.

The hearing aid of the present invention is designed so that the gain of the second formant is raised without raising the gain of the first formant, which keeps the clarity of voices high without their sounding too loud. A state in which even the first formant cannot be heard is not under discussion here, in which case it is necessary to perform overall amplification so that the first formant can be heard, and raise the gain of the second formant.

The level of the first formant in conversation is usually about 50 to 60 dB, which is high, and even people with mild to moderate deafness can still hear adequately, but because the level of the second formant is about 20 to 40 dB lower than that of the first formant, voices will not seem too loud even if the second formant is boosted to about this same level.

Therefore, not raising the gain of the first formant and raising the gain of the second formant makes voices become clear, and since the gain of the first formant does not change, the voices do not sound loud.

Figure 1 consists of graphs of the operating condition settings of the hearing aid pertaining to

the present invention. The horizontal axis is frequency, and the vertical axis is the SPL. Fig. 1A shows the frequency spectrum related to the vowel "I" seen in Figure 8, and Fig. 1B shows the frequency

5   spectrum related to the vowel "A" seen in Figure 8.

For example, if a person cannot hear sounds below an SPL of 50 dB, then, as is obvious from Figure 1A, that person can only hear the first formant with the vowel "I" and cannot tell which

10   sound it is, further since he can faintly hear the second formant with the vowel "A" as shown in Fig. 1B, he can tell that the sound is "A", although he will be uncertain if the voice is a little softer.

With the hearing aid pertaining to the present

15   invention, as shown by the broken line in Figure 1A and 1B, the first formant is not amplified, and just the second formant is amplified enough to reach the required level, thus bringing both the first formant and second formant within the audible range.

20   With the "I" sound in Figure 1A, frequencies of the 350 Hz frequency of the first formant and higher are corrected by 6 dB/oct up to a maximum of 20 dB.

This correction strengthens the second formant (2.7 kHz, SPL of 42 dB) by 18 dB, bringing it up to

25   SPL of 60 dB, so a person who cannot hear below an SPL of 50 dB can adequately catch the first and second formants and is able to tell that the sound is

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"I." The corrected frequency spectrum is indicated by a one-dot chain line in Figure 1A.

With the "A" sound in Figure 1B, frequencies of the 1 kHz frequency of the first formant and higher are corrected by 6 dB/oct up to a maximum of 20 dB.

With the sound "A," even without correction, a person who cannot hear below an SPL of 50 dB can tell that the sound is "A" if he pays close attention, since the second formant is 53 dB, but the level rises to SPL 57 dB with correction, which allows the sound to be heard more clearly. Again in Figure 1B, the corrected frequency spectrum is indicated by a one-dot chain line.

A feature of the correction characteristics in the hearing aid of the present invention is that they change in relation to the change in the first formant frequency. In the past, when frequency characteristics were corrected by tone control or the like, the correction characteristics themselves did not change when the first formant changed.

For instance, when a conventional tone control is used to set the correction characteristics to match the frequency spectrum of the sound "I" seen in Figure 1A (that is, the correction characteristics indicated by the broken line of Fig. 1A), and the wearer hears the sound "A" in this state, 1 kHz, which is the first formant of the sound "A" as shown

in Fig. 1B, is strengthened by 10 dB, bringing the SPL of first formant up to 80 dB and making the sound "A" 10 dB louder than the sound "I." This results in a so-called ringing noise because the degree of

5   amplification for first formant rises along with the frequency of the first formant rises as the sound "A".

Because the extent of hearing impairment can vary widely, correction of a hearing aid must be matched to the extent of impairment of the user, and

10   therefore the amount of correction must be matched to the user, and cannot be fixed.

When correction is thus tailored to the extent of impairment of the user, if the user cannot hear even the first formant, then first of all

15   amplification must be performed for all frequencies up to the level where the first formant can be heard, and then the corrective amplification for the second formant pertaining to the present invention must be performed.

20   The first and second formants described above are the minimum elements required to understand language, and useful information is also contained in the third, fourth, and subsequent formants, so reproducing these is also important, and since these

25   are contained in substantially higher frequencies than the first formant, the correction pertaining to the present invention is effective with them as well.

The above description is focused primarily on language, but being able to hear frequencies over the first formant is effective for musical notes and all information obtained from sound waves and required in

5   our daily lives, and makes it possible to obtain more information.

Because of the above, first aspect of the present invention is a hearing aid for amplifying an acoustic signals:

10   (1) comprising:

a controller for determining in real time a frequency band at the highest level of the acoustic signals through frequency analysis of the acoustic signals that vary over time, and for generating a

15   control signal to raise a gain for signals of a higher frequency range than the frequency band at the highest level (such as an amplifier Q3, or a band-pass filter group 2 and a diode matrix 3 and a comparator 4, or a digital signal processor 13, or

20   the like); and

a first amplifier, in which the control signal from said controller is inputted so that the frequency characteristics are varied, for amplifying the acoustic signals by increasing the gain for

25   signals of the higher frequency range than the frequency band at the highest level (such as an amplifier system consisting of amplifiers Q1 and Q2,

or a parametric equalizer 5, or a digital signal processor 13, or the like), or

(2) in (1) above, the controller comprising a second amplifier whose gain is a function of the frequency (such as the amplifier Q3), or

(3) in (1) above, the first amplifier, comprising an amplification apparatus (such as an amplification apparatus including amplifiers Q1 and Q2) in which a plurality of sub-amplifiers with different frequency characteristics, each capable of gain control, are connected in parallel, and the outputs of the plurality of sub-amplifiers are added together, or

(4) in (1) above, the controller comprising a band-pass filter group (such as the band-pass filter group 2), a diode matrix (such as the diode matrix 3), and a comparator group (such as the comparator group 4), or

(5) in (1) above, the first amplifier, comprising a parametric equalizer, or

(6) comprising:

an A/D converter provided on the side where the acoustic signals are inputted, for converting analog signals of the acoustic signals into digital signals (such as an A/D converter 12);

a digital signal processor for determining in real time a frequency band at the highest level of

the digital signals through frequency analysis of the digital signals that are outputted from the A/D converter and vary over time, and then for generating a control signal for raising a gain for signals of a

5   higher frequency range than the signal of the frequency band at the highest level, and then for amplifying the digital signals by increasing the gain for signals of the higher frequency range than the frequency band at the highest level, according to the

10   control signal; and

a D/A converter for converting the digital signals outputted from the digital signal processor into analog signals (such as a D/A converter 14).

The adoption of the above structure results in a

15   hearing aid which amplifies an input acoustic signals so that all sounds can be clearly understood but do not sound overly loud.

The second aspect of the present invention is a hearing aid for amplifying an input acoustic signals

20   that vary over time comprising:

a control circuit for generating a control signal according to a first frequency band at the highest level of the input acoustic signals; and

an amplifier for amplifying the input acoustic

25   signals so as to generate an output acoustic signals, wherein the amplifier has a frequency characteristic including a first gain region which has a constant

gain for frequencies equal to or lower than the first frequency band, and a second gain region whose gain increases higher than the first gain region, according to frequency, for frequencies higher than

5   the first frequency band; and in response to the control signal, an increase point between the first and second gain regions changes according to the first frequency band.

The frequency characteristic for the gain is

10   dynamically controlled depending on the first frequency band at the highest level of the input acoustic signals so that the increase point between the flat gain region and the increasing gain region changes dynamically.

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BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1A and 1B are graphs of the operating condition settings of the hearing aid pertaining to

20   the present invention;

Fig. 2A and 2B are diagram illustrating an amplification system for constituting Embodiment 1 in the present invention;

Fig. 3 is a diagram illustrating first formant

25   frequency detection by the amplifier Q3 seen in Fig. 2;

Fig. 4 is a block diagram of the main elements

and serves to illustrate the hearing aid in
Embodiment 2 of the present invention;

Fig. 5A and 5B are graphs illustrating the
characteristics of the main structural elements in
the hearing aid seen in Fig. 4;

Fig. 6 is a block diagram of the main elements
and serves to illustrate the hearing aid in
Embodiment 3 of the present invention;

Fig. 7 is a graph of equisignal curves of the
loudness of sound in humans with normal hearing;

Fig. 8 is a graph of the formants of Japanese
vowels; and

Fig. 9 Figure 9 is a table of typical values for
various sounds and their corresponding formant
frequencies.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

The hearing aid pertaining to the present
invention should have an amplification system that
allows the principle of the present invention as
described above to be realized, and while this
amplification system must be one with which the
frequency characteristics can be varied, many
conventional means are known for varying the
frequency characteristics.

Figure 2 is a diagram illustrating an

amplification apparatus for constituting Embodiment 1
in the present invention. Fig. 2A is a graph of the
frequency characteristics and Fig. 2B is a block
diagram of the structure of the amplification

5   apparatus. An input acoustic signal IN amplified by
Q1 and Q2 to generate an output signal OUT.

In the figures, Q1 is an amplifier having the
frequency characteristics seen in (1) of Figure 2A,
Q2 is an amplifier having the frequency

10   characteristics seen in (2) of Figure 2A, Q3 is an
amplifier that controls the amplifier Q2, OT is an
output terminal of the amplification apparatus, and β
is the corrected gain of the amplifier Q2.

The amplification apparatus consists of the

15   amplifiers Q1 and Q2 connected in parallel, and the
amplifier Q3 that controls the corrected gain β of
the amplifier Q2. The combined output of the
amplifiers Q1 and Q2 is outputted from the output
terminal OT.

20   The amplifier Q2 is designed so that its gain is
controlled to be varied acccording to the output
corresponding to the first formant frequency from the
amplifier Q3, and the frequency characteristics seen
in (3), (4), and (5) of Figure 2A can be achieved.

25   That is, when β is controlled to be 10 dB, the
frequency characteristics is (3), when β is
controlled to be 20 dB, it is (4), and when β is

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controlled to be 30 dB, it is (5).

The characteristics of the amplifier Q1 are dominant if the gain of the amplifier Q2 + β is low, but the characteristics of the amplifier Q2 + β are dominant if the gain of the amplifier Q2 + β exceeds the gain of the amplifier Q1 over the entire frequency band, between which the gain varies smoothly and the frequency at which the gain correction for higher frequency begins varies from (3) to (5) depending on the first formant frequency, so this is favorable as the characteristic correction amplification system of the present invention.

As can be seen from Figure 2, the characteristics of the amplifier Q2 are corrected by 20 dB between 200 Hz and 2 kHz, but the amount of correction should be determined according to the level of the person who is hard of hearing, and is not limited to 20 dB.

Figure 3 is a diagram illustrating first formant frequency detection by the amplifier Q3 shown in Figure 2. The horizontal axis is frequency, the left vertical axis is gain, and the right vertical axis is output level.

It is clear from the characteristics lines indicated by the symbol Q3 in Figure 3 that the amplifier Q3 is one in which gain increases linearly by 6 dB/oct, and when a voice signal is added, the

degree of amplification increases and output goes up as the first formant frequency rises.

That is, when the input signal of vowel "I" is supplied to the amplifier Q3, since the gain for the frequency of the first formant of "I" is lower, the output of the amplifier Q3 is automatically lower so that β of the amplifier Q2 is controlled to be higher. On the other hand, when the input signal of vowel "A" is supplied to the amplifier Q3, since the gain for the frequency of the first formant of "A" is higher, the output of the amplifier Q3 is automatically higher so that β of the amplifier Q2 is controlled to be lower. Therefore, the amplifier Q3 virtually detects a first formant frequency of the input acoustic signals, then generates a control signal to change β of the amplifier Q2.

As described for Figure 2, this output of Q3 changes the characteristics of the amplification system (Q1 + Q2 + β). Specifically, it results in the following.

First formant frequency:

250 Hz or lower: the characteristics (5) in Figure 2A

600 Hz: the characteristics (4) in Figure 2A

2 kHz or higher: the characteristics (3) in Figure 2A

According to the above explanation, when the

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first formant frequency is lower, the total gain of the amplification system increases from a lower frequency as (5). And, when the first formant frequency is higher, the starting frequency for gain increases is higher as (4), (3).

As explained above, the amplification system (Q1+Q2+β) has a frequency characteristic including a first gain region which has a constant gain for frequencies equal to or lower than the frequency band of the first formant, and a second gain region whose gain increases higher than the first gain region, according to frequency, for frequencies higher than the frequency band of the first formant; and an increase point between the first and second gain regions changes according to the frequency band of the first formant. The frequency of the first formant can be detected as the frequency band of the highest level signal. The increase point becomes higher when the frequency band of the highest level signal becomes higher, and the increase point becomes lower when the frequency band of the highest level signal becomes lower. Such increase point changes in response to the control signal generated by the amplifier Q3.

The hearing aid described for Figures 2 and 3 is a simple model made up of analog circuitry, but since it is practical, there is no delay in signal

processing attendant to digital processing, and there is no omission of very faint signals of 1 bit or less; the location of a sound source can be accurately recognized when the hearing aid is used in both ears, so that the surrounding situation can be assessed by sound.

Figure 4 is a block diagram of the main elements and serves to illustrate the hearing aid in Embodiment 2 of the present invention. In this figure, 1 is an input amplifier, 2 is a band-pass filter group, 3 is a diode matrix, 4 is a comparator group, 5 is a parametric equalizer (parametric amplifier), and 6 is an output amplifier. The band-pass filter group 2 is made up of band-pass filters F1, F2, F3, and F4, and the comparator group 4 is made up of comparators C0, C1, C2, C3, and C4.

Figure 5A and 5B are graphs illustrating the characteristics of the main structural elements in the hearing aid seen in Figure 4. Fig. 5A is a graph of the characteristics of the band-pass filters, and Fig. 5B is a graph of the characteristics of the parametric equalizer. In both graphs, the horizontal axis is frequency and the vertical axis is degree of amplification. The symbols appended to the characteristic lines correspond to the characteristics of the elements in Figure 4 labeled with the same symbols. f_1, f_2, f_3, and f_4 are the

center frequencies of the band-pass filters F1, F2, F3, and F4.

It is well known that the comparators C1 to C4 in the hearing aid seen in Figure 4 compare the voltage of two input terminals and generate their output. If the voltage of the positive terminal is greater than that of the negative terminal, the output will be positive, otherwise the output will be negative.

If the output voltage of the band-pass filter F2 is greater than the output voltage of the other band-pass filters, then the output of the comparators is determined by the comparator terminal to which the voltage of the band-pass filter F2 is applied.

For instance, the voltage from the band-pass filter F2 is applied to the positive terminal with the comparator C2, but with the other comparators C1, C3, and C4, it is applied to the negative terminal, according to the action of the diode matrix 3 so if the output voltage of the band-pass filter F2 is higher than the output of the other band-pass filters, just the output of the comparator C2 becomes positive, and the output of the other comparators becomes negative.

Therefore, if the highest signal level of the input signal has the center frequency f_2 of the band-pass filter F2, or a frequency close thereto, the

output of the comparator C2 becomes positive, and if the highest signal level of the input signal has the center frequency f_3 of the band-pass filter F3, or a frequency close thereto, the output of the comparator C3 becomes positive.

It is a well-known fact that a parametric equalizer, that is, a parametric amplifier, can vary characteristics from the outside, and the parametric equalizer 5 shown in Figure 4 serves to raise the degree of amplification of frequencies higher than the center frequency f_1 when the output of the comparator C1 is positive, as seen in Figure 5B.

Similarly, it serves to raise the degree of amplification of frequencies higher than the center frequency f_2 when the output of the comparator C2 is positive, to raise the degree of amplification of frequencies higher than the center frequency f_3 when the output of the comparator C3 is positive, and to raise the degree of amplification of frequencies higher than the center frequency f_4 when the output of the comparator C4 is positive.

The frequency characteristics in the hearing aid of Figure 4 may be any of the characteristics of the parametric equalizer 5 seen in Figure 5B, and which characteristics they become is determined by the input signals.

If the level of the input signal is lower than

the specified level, the output of the comparator CO
becomes positive, the characteristics of the
parametric equalizer 5 become CO in Figure 5B, and
just the frequencies higher than f_0 are amplified,
but if the input signal is over the specified level,
the characteristics are determined by the frequency
with the most energy out of the frequencies included
in the input signal. For instance, if this frequency
is f_1, then frequencies lower than f_1 are not
amplified, and just those frequencies higher than f_1
are amplified.

Similarly, if the frequency is f_2, f_3, or f_4,
then frequencies lower than f_2, lower than f_3, or
lower than f_4 are correspondingly not amplified, and
only input signals whose frequency is higher than
these are amplified.

In the descriptions above, the frequency band
being used is divided up into four bands for easy
understanding, but one band generally consists of one
third of an octave or one sixth of an octave.

Therefore, in the case of 300 to 2400 Hz (3
octaves), the frequency would be divided into 9 or 18
bands, and even when the frequency is thus divided
into numerous bands, band-pass filters can be easily
configured as active filters with existing integrated
circuit technology, and even the comparators and
parametric equalizer can be easily integrated

together with them.

The slope of the correction characteristics in the hearing aid of the present invention is generally 6 dB/oct or 12 dB/oct, and the maximum amount of correction is 20 to 30 dB, but these refer to correcting the characteristics of the user's ear, and since there are individual differences, optimal results will be obtained by tailoring these values to the individual.

Incidentally, electronic devices that are extremely useful in carrying out the acoustic signal processing required for the hearing aid have now become practical, an example of which is a digital signal processor (DSP). A DSP can be programmed to operate as a variety of electronic devices, such as a spectrum analyzer or a parametric equalizer.

Figure 6 is a block diagram of the main elements and serves to illustrate the hearing aid in Embodiment 3 of the present invention. In this figure, 11 is an input amplifier, 12 is an A/D converter, 13 is a DSP, 14 is a D/A converter, and 15 is an output amplifier.

With this hearing aid, the input signal is passed through the input amplifier 11 so as to maintain the first formant frequency at a specific audible level, this amplified signal is digitized by the A/D converter 12, and this digital signal is

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inputted to the DSP 13.

By preprogramming the DSP 13, it can act as a
spectrum analyzer to perform frequency analysis, the
digital data thus obtained is computed, and this DSP
13 then acts as a parametric equalizer to amplify and
correct just the signals of the second formant
frequency and send out a signal.

The signal corrected and amplified by the DSP 13
is converted back into an analog signal by the D/A
converter 14, and reaches the ear of the user after
being suitably amplified by the output amplifier 15.

The hearing aid pertaining to the present
invention comprises a controller for determining in
real time a signal with a frequency band at the
highest level of the acoustic signals through
frequency analysis of the acoustic signals that vary
over time, and for generating a control signal to
raise a gain of signals of a higher frequency range
than the signal of the frequency band at the highest
level, and a first amplifier, in which a control
signal from the controller is inputted so that the
frequency characteristics are varied, for amplifying
the acoustic signal by increasing the gain for
signals of the higher frequency range than the signal
of the frequency band at the highest level.

The adoption of the above structure results in a

hearing aid which amplifies all sounds so that they can be clearly understood but do not sound overly loud.